|  |
| --- |
| IALA Guideline |

DRAFT

Marine signal lights

Calculation of Luminous intensity and range

Edition x.x

Document date

Revisions to this IALA document are to be noted in the table prior to the issue of a revised document.

|  |  |  |
| --- | --- | --- |
| Date | Page / Section Revised | Requirement for Revision |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

1. Acronyms 7

2. Aims 7

3. Introduction 7

4. Physical basics 7

4.1. Luminous intensity 7

4.2. Illuminance 7

4.3. Meteorological visibility 7

4.4. Allard’s law 7

4.5. Luminous intensity calculations 8

4.5.1. Minimum luminous intensity 8

4.5.2. Maximum luminous intensity 8

4.5.3. Design intensity 8

5. Key values 9

5.1. Minimum illuminance at the observer’s eye 9

5.2. Measuring background illuminance 10

5.3. Maximum illuminance at the eye of the observer 10

5.4. Minimum meteorological visibility 11

5.5. Maximum meteorological visibility 11

6. Rival lights 11

6.1. Illumination of areas, roads and buildings 12

6.2. Navigation lights on vessels 12

6.3. Other signal lights 13

7. PHOTOMETRIC LUMINOUS INTENSITY 15

7.1. In-Situ- and Photometric Intensity 15

7.2. Steady burning lights 16

7.3. fast Switching lights 16

7.4. Arbitrary Flash Profile 16

8. Standard Design Methodology 17

8.1. Step 1 17

8.2. Step 2 17

8.3. Step 3 17

8.4. Step 4 17

8.5. Step 5 17

8.5.1. Steady burning light 17

8.5.2. Fast switching light (rectangular flash profile, LED) 17

8.5.3. Lights with arbitrary flash profile 18

9. Examples FOR INTENSITY CALCULATIONS 18

9.1. Example 1 18

9.1.1. STEP 1 18

9.1.2. STEP 2 18

9.1.3. STEP 3 18

9.1.4. Step 4 18

9.1.5. Step 5 18

9.1.6. Result 19

9.2. Example 2 19

9.2.1. STEP 1 19

9.2.2. STEP 2 19

9.2.3. STEP 3 19

9.2.4. STEP 4 20

9.2.5. STEP 5 20

9.2.6. Result 20

9.3. Example 3 20

9.4. Example 4 20

9.5. Example 5 20

10. LUMINOUS RANGE CALCULATION 21

10.1. Calculation process 21

10.1.1. Newton-Raphson method 21

10.1.2. Application to luminous range calculation 22

10.2. Nominal Range 22

10.3. Parametric luminous range 23

10.4. Examples 23

List of Tables

**Es konnten keine Einträge für ein Abbildungsverzeichnis gefunden werden.**

List of Figures

**Es konnten keine Einträge für ein Abbildungsverzeichnis gefunden werden.**

List of Equations

Equation 1 Allard’s law 7

Equation 2 Luminous intensity calculation 8

Equation 3 Minimum luminous intensity 8

Equation 4 Maximum luminous intensity 8

Equation 5 Design luminous intensity 8

Equation 6 as a function background luminance 12

Equation 7 Recommended values for minimum meteorological visibility 14

Equation 8 Inequation for the intensity of a marine light considering a rival light 17

Equation 9 in-situ-intensity, steady burning lights, design values 21

Equation 10 In-situ-intensity, steady burning lights, minimum values 21

Equation 11 In-situ-intensity, steady burning lights, maximum values 21

Equation 12 In-situ-intensity, fast switching light, minimum values 21

Equation 13 In-situ-intensity, fast switching light, maximum values 21

Equation 14 Allard’s Law 26

Equation 15 Function F 26

Equation 16 Range as the root of function F 27

Equation 17 First step 27

Equation 18 Step n+1 27

Equation 19 Final step 27

Equation 20 Derivative 27

Equation 21 Allard’s Law, physical presentation 29

Equation 22 Transmissivity (luminous flux) 29

Equation 23 Transmissivity (illuminance) 29

# Acronyms

FILL WITH ACRONYMS

# Aims

The aim of this guideline is to give information about the calculations necessary to derive the luminous intensity of an AtoN light from the navigational requirements.

# Introduction

A suitable luminous intensity is one of the basic features of a light. The intensity should be high enough to ensure that the light is visible for navigation as required. It should not be too bright to avoid glare.

Normally the operating expense is strongly influenced by the luminous intensity. A 10-cd-light can be realized by a cheap and small lantern immediately available from stock of a manufacturer. A sector light of about 1 000 000 cd will require a special design and will be produced for a single position.

# Physical basics

## Luminous intensity

The brightness of the light emitted by a signal lantern is expressed with the luminous intensity . The unit is Candela (cd [1]). ‘Luminous intensity‘ and ‘luminous range’ are abbreviated to ‘intensity’ and ‘range’ in some chapters of this guideline.

## Illuminance

The brightness of the light seen by a distant observer is expressed with the illuminance . The unit is Lux (lx [1]).

## Meteorological visibility

The light emitted is attenuated by absorption and scattering in the atmosphere. This attenuation is specified by the ‘meteorological visibility’. Its unit is metres or nautical miles (1 852 metres = 1 nautical mile).

Although meteorological visibility is described by a distance or length, its value does not represent a range to determine the useful distance of a light or a daymark.

There are other ways to describe the attenuation of the atmosphere. These are shown in the Annex.

## Allard’s law

Allard’s law allows the calculation of the illuminance as a function of distance, luminous intensity and the meteorological visibility.

Equation 1 Allard’s law

Where:

is the illuminance at the eye of the observer

is the luminous intensity

is the distance between the light and the observer

is the meteorological visibility (), see IALA dictionary



Figure 1 Quantities for Allard’s law

## Luminous intensity calculations

Rearranging Equation 1 gives an equation to calculate the luminous intensity of a marine signal light.

Equation 2 Luminous intensity calculation

FURTHER EXPAINATION IS REQUIRED HERE (DIAGRAM OF ZONE OF UTILISATION)

### Minimum luminous intensity for the

The calculation of the required luminous intensity of a marine signal light is based on the input of

* the maximum distance the light will be used,
* the required minimum illuminance at the eye of the observer,
* and a local conditions value for the meteorological visibility .

The luminous intensity calculated will be the minimum required luminous intensity .

Equation 3 Minimum luminous intensity

Whereas the maximum distance varies with each light and its position to the waterway, there are values recommended for the illuminance and the meteorological visibility.

### Maximum luminous intensity

At a short distance a light may appear very bright and it may even cause glare. To avoid this, a maximum luminous intensity should be defined. This can be calculated by Allard’s law and

* the minimum distance the light will be used,
* the maximum acceptable illuminance at the eye of the observer to avoid glare
* and a maximum value for the meteorological visibilty .

Equation 4 Maximum luminous intensity

### Design intensity

The calculation of the minimum and maximum luminous intensity normally gives an interval the real intensity should be between:

In many cases the interval is very large . To reduce the expense for a light it is recommended to link the intended luminous intensity during design procedure of a light to the minimum value . However there should be some safety factor between the minimum intensity and the design intensity . It is recommended to choose this factor to 1.2x.

Equation 5 Design luminous intensity

In a few cases the calculated minimum may become larger than the maximum . In that case it has to be decided whether glare at a near position of the observer is accepted or the intensity may be reduced.

ARE THERE OTHER MEASURES TO BE CONSIDERED?

# Key values

Beside the maximum and minimum distance the light will be used as an Aid to Navigation, the intensity calculations requires input values for maximum and minimum illuminance and meteorological visibility.

## Minimum illuminance at the observer’s eye

For many years marine signal lights were designed for situations without any additional disturbing lights. The situation has changed and additional lights, interfering with the signal light, have to be considered. The influence of additional lights can be divided in two different aspects.

* background illumination : smooth halo of light produced by scattered light
* rival lights : appearing as point lights, directly emitted to the observer



background illumination

rival

lights

leading line

buoys

Figure 2 Marine signal lights, background illumination and rival lights

The influence of background illumination is covered by adjusting the minimum illuminance at the eye of the observer.

Rival lights are treated in this document at a later step (See Chapter 6).

The minimum illuminance at the eye of the observer depends on the background illumination found at the position of the light. Traditionally the values in Table 1 are used to define the minimum illuminance.

Table 1 Minimum illuminance at the eye of the observer

|  |  |  |
| --- | --- | --- |
| Background | Relevant lights |  |
| Lights for nighttime use |  |  |
| - no background illumination | all lights except leading lights |  |
| - no background illumination | leading lights |  |
| - minor background illumination | all lights |  |
| - substantial background illumination | all lights |  |
| Lights for daytime use | all lights |  |

Although it is still acceptable to use the table, there are two aspects, which may require a more detailed investigation.

* The definition of the background is not based on physical quantities and cannot be measured. It is only based on the estimation of an observer (mariner).
* The ratio between the different values for the illuminance is 10 and therefore the minimum luminous intensity may increase by a factor 10 or 100, when it is assumed to have background illumination. This may lead to very intense and expensive lights. This can be solved byusing the equation 6.

A formula for the calculation of the required illuminance as a function of the background luminance has already been used for many years. Its main purpose was for daytime lights only. However the values of the formula fit very well to the existing values, so it can be interpreted as an interpolation of these values.

Equation 6 as a function background luminance

Where:

is the background illuminance near the light in

INSERT REFERENCE

Remark:

There is a difference about 20% when the value is calculated from Equation 6 with or drawn from Table 1. It is suggested that with no background illumination the value is used and if background illumination is considered and can be measured () Equation 6. If the illumination cannot be measured the values of table 1 should be used.

## Measuring background luminance

The background luminance can be measured with a luminance meter. A luminance meter has an ocular where the object to be measured is marked by a circular reticle. The luminance of the surface inside the reticle is measured.



reticle

leading line

halo

Figure 3 Measuring background luminance

Measurement procedure should take into account that

* the meteorological visibility has a medium value of 4 to 10 M during measurement,
* the measuring field (reticle) should be placed nearby the signal light,
* the measuring field (reticle) should not contain rival lights (point lights),
* the measuring field (reticle) should be illuminated uniformly
* the measurement distance should be near the minimum distance .

## Maximum luminance at the eye of the observer

The maximum illuminance is defined in Table 2 with two values depending on background illumination.

Table 2 Maximum illuminance at the eye of observer

|  |  |
| --- | --- |
| background illumination |  |
| * none | 0.01 |
| * present | 0.1 |

## Minimum meteorological visibility

The nominal range of a light is defined for a meteorological visibility of 10 nautical miles (18 520 m). However, in many regions this visibility does not occur for a long period, so the light may be not visible at maximum distance.

To improve the visual performance of a light, it is recommended to use a local conditions visibility for the intensity calculations, which may be lower than 10 M.

Competent authorities should choose a value for a local conditions visibility based on:

* Meteorological historical data
* User experience

The competent authority should choose a value (SOMETHING with Percentage)

may wish to to use a value which is lower than the local conditions value depending on the degree of risk associated with the light.

ADD POSSIBLE INPUTS FOR CHOOSING VISIBILITY.

Examples:

PLEASE PROVIDE EXAMPLES HOW TO CHOOSE VISIBILITY

FRANK HERMANN, FERNANDO ROMERO, BRAZIL VALUES ON THE WIKI

## The competent authority should choose a percentile value from the historical meteorological data depending on the degree of risk associated with the light. For example, a meteorological visibility of 18NM or greater for 90% of the time may be appropriate for a particular location. This may result in a light with a published nominal range of 19NM.  At another location where navigation is more difficult (degree of risk is higher) a meteorological visibility of 18NM or greater for 50% of the time might be more appropriate. This may result in a light with a published nominal range of 20NM.Maximum meteorological visibility

The maximum visibility is used to estimate glare from a near position. In a ‘worst case scenario’ this calculation should be done for a very good meteorological visibility.

is the preferred value for this purpose.

Some administrations use ‘infinity’ instead (). In this case Allard’s law cannot be used, but .

# Rival lights

With the calculation described in chapter 4 and 5, an intensity for the marine signal light is determined. However there may be other lights (rival lights) in the vicinity of the marine signal light, showing the same or a higher intensity.

This may influence the recognisability of the marine signal light.

Rival lights may be:

* illumination of ports, roads and buildings,
* navigation lights on vessels,
* aeronautical lights,
* road traffic lights,
* other marine signal lights.

## Illumination of areas, roads and buildings

These lights should have a light cone (luminous intensity distribution) which covers the illuminated surface only. When done properly, there will be no direct light into the direction of the waterway. Only scattered light should be visible, which is added to the background illumination (halo).

However, in many situations there will be some direct light pointing into the direction of the waterway and interfering with a marine signal light (Figure 4).



Figure 4 A rival light

In that case the operator of the illumination equipment should be contacted and measures should be taken to remove the direct light.

This can be done either by rotating the lantern to move the light cone away from the waterway or by introducing cut-off-screens (Figure 5).



Figure 5 Using a cut-off-screen to remove direct light

## Navigation lights on vessels

The navigation lights on vessels are defined by IMO COLREGs, Rule 22 and Annex I [2]. In many situations navigation lights (on a vessel) and marine signal lights (light house, beacon, buoy) may be easily distinguished by the flash characters, as navigation lights normally are steady burning lights and signal lights are flashing.

However, this is not always true and therefore it makes sense to look at the intensities of the navigation lights and harmonize them with the signal lights.

The top light of a navigation light is the most intense light on a vessel and its luminous intensity is linked to the length of a vessel.

Table 3 Luminous intensity of navigation lights on vessels

|  |  |  |
| --- | --- | --- |
| length of a vessel | luminous intensity (white, top) | luminous intensity (green, red) |
| L < 12 m | approx. 4.3 cd | 0.9 cd |
| 12 m ≤ L < 50 m | 12 - 52 cd | 4.3 cd |
| L ≥ 50 m | approx. 94 cd | 12 cd |

Remark: IMO does not use the IALA definition on nominal range.

To compete with navigation lights, there should be a minimum luminous intensity defined for a marine signal light.

It is recommended that the luminous intensity of a marine signal light should not be less than the minimum value given in Table 4. For example, when a minimum intensity for a lighted buoy is calculated, the value should be replaced with .

Table 4 Minimum luminous intensity of a marine signal light

|  |  |
| --- | --- |
| Type of light | minimum luminous intensity |
| Lights on a buoy | 5 cd |
| Beacon / Light house | 10 cd |
| Leading Light | 50 cd |

## Other signal lights

Aeronautical lights, road traffic signal lights and other marine signal lights may cause confusion with the signal light, the calculations are done for.

If it is not possible to remove direct light, which is going to the waterway, the intensity of the marine signal light may be increased beyond the design intensity (chapter 4.5.3).

An example is shown in Figure 6. The marine light is a sector light with three sectors. The coloured area shows the positions the sector light is used by the mariners. Next to the marine light there is a high intensity aeronautical light.

To ensure that the marine signal light will compete with the aeronautical light, the illuminance of the marine light should be at least the same as for the aeronautical light. The calculation should be done with Allard’s law with the local conditions visibility chosen in chapter 5.3. and some relevant positions.



Figure 6 Intensity check for a rival aeronautical light

In the example the observer is on a vessel in the white sector. The distance to the sector light is (marine light) and to the aeronautical light is (rival light).

The illuminance at the eye of the observer produced by the marine light at minimum visibility is:

.

The illuminance at the eye of the observer produced by the aeronautical light at minimum visibility is:

.

The illuminance produced by the marine light should be equal or greater than the illuminance of the aeronautical light:

.

This gives the inequation:

.

Rearranging the formula gives a minimum value for the luminous intensity of the marine signal light.

Equation 8 Inequation for the intensity of a marine light considering a rival light

.

The luminous intensity of the rival light has to be reported by the operator.

Some typical values are given in Table 5.

Table 5 Intensity of road traffic and aeronautical signal lights at night

|  |  |  |  |
| --- | --- | --- | --- |
| Purpose | Type | Luminous intensity | Characteristics |
| Aeronautical obstacle lights [3] | Low-intensity, Type A, red, fixed | 10 cd | omnidirectional |
| Low-intensity, Type B, red, fixed | 30 cd | omnidirectional |
| Medium intensity, Type A, white, flashing | 2000 cd | omnidirectional |
| Medium intensity, Type B,  red, flashing | 2000 cd | omnidirectional |
| Road traffic lights [4] | Green, Red, Yellow | 25 - 200 cd | pencil beam |

# PHOTOMETRIC LUMINOUS INTENSITY

## In-Situ- and Photometric Intensity

The luminous intensity calculated in the chapters above is an intensity, which should be guaranteed, when the light is in operation. It is called in-situ-intensity in this chapter.

It is not the luminous intensity, which is measured in a light laboratory. The measured intensity is now called photometric intensity .

Two aspects have to be considered.

* A service condition factor   
  This factor includes the degradation of the luminous intensity caused by the aging of the light source, and dirt or salting of the lanterns.  
  The service condition factor is used for the minimum intensity values only. The maximum intensity is estimated for a ‘worst-case-scenario’ (avoid glare) and therefore it should estimated that the lantern was not aged and has the full intensity.  
  For many years IALA proposed to assume that the intensity reduction should be taken as 25% of the measured value in a laboratory ().
* The flash characters  
  Many lights are measured with fixed light and operated with different flashes. As the effective intensity depends on the flash character, it has to be calculated from the variation in time of the luminous intensity.

The measured luminous intensity of a signal light is now called photometric luminous intensity . It may vary with the horizontal and vertical angle and with time .

viewing distance

*D*

Allard’s Law

in-situ-

intensity *Iins*

service condition

flash profile

photometric

intensity *Iph*

Figure 7 Calculation process from distance to photometric intensity

## Steady burning lights

For steady burning lights the in-situ-intensity can be calculated from the nominal photometric intensity with:

Equation 9 In-situ-intensity, steady burning lights, design values

Equation 10 In-situ-intensity, steady burning lights, minimum values

(with intensity reduction, service condition)

As stated before the maximum value for the intensity is based on a ‘worst-case-scenario’, which assumes that the lantern is new. Therefore the service condition factor is not included or taken as ‘1’.

Equation 11 In-situ-intensity, steady burning lights, maximum values

(without intensity reduction)

## fast Switching lights

For a fast switching light the flash profile has a rectangular shape. For example, a flashing light shows two flashes (1) and (2) with different size (Figure 8).



Figure 8 Rectangular flash shape

The length of the shortest flash in seconds is used to calculate the apparent intensity and then the in-situ-intensity of the light (the formula uses a time constant ).

Equation 12 In-situ-intensity, fast switching light, minimum values

Equation 13 In-situ-intensity, fast switching light, maximum values

## Arbitrary Flash Profile

For an arbitrary flash profile the profile function must be known. There are tools (e.g. Modified Allard, Schmidt-Clausen, Blondel-Ray-Douglas) to calculate the in-situ-intensity from the profile function.

# Standard Design Methodology

The standard procedure to derive the required luminous intensity or intensity distribution from the nautical requirements is shown in this chapter.

When a light has sectors with different distances and , it may be useful to repeat the calculations for each sector. When the differences between the sectors are not too large, the calculation may be done with the largest value of and the lowest for .

## Step 1

Find the nautical requirements of light, which are described by

* the flash (minimum flash duration is ),
* the minimum distance ,
* the maximum distance ,

## Step 2

Fix the essential parameters for calculation.

* minimum illuminance at the eye of the observer
* maximum illuminance at the eye of the observer
* minimum meteorological visibilty

## Step 3

Calculate the in-situ-intensity with Allard’s law.

* minimum :
* maximum : with ()
* design :

## Step 4

Check for rival lights. If rival lights have to be considered, estimate a new minimum intensity according to chapter 6.

## Step 5

Calculate the photometric intensity.

### Steady burning light

with .

### Fast switching light (rectangular flash profile, LED)

with and .

### Lights with arbitrary flash profile

Use the concept of effective intensity to estimate the photometric luminous intensity.

# Examples FOR INTENSITY CALCULATIONS

## Example 1

A light with a maximum viewing distance of about has to be designed. There is no background illumination an the minimum visibility is assumed to be . The flash character is Iso 3s.

### STEP 1

* the flash character Iso 3s has and an eclipse of
* the minimum distance is ,
* the maximum distance is .

### STEP 2

As there is no background light the following values for the illuminance at the eye of the observer are chosen.

* minimum illuminance
* maximum illuminance
* minimum visibility .

### STEP 3

Calculate the in-situ-intensity with Allard’s law.

* minimum :
* maximum :
* design :

### Step 4

At the fairway no rival lights were to be considered and therefore the intensity is not adjusted.

### Step 5

Photometric luminous intensity:

With and the photometric values are:

* minimum :
* maximum :
* design:

### Result

The lantern should have a photometric luminous intensity of approx. . The required minimum intensity is .

## Example 2

A lantern for a small light buoy should be defined by its luminous intensity. The fairway is used by small vessels only and the required viewing distance is about 1 M. There is no background illumination. The flash character is Fl 4s and fast switching LED should be used.

### STEP 1

* the flash character Fl 4s will be realized with and an eclipse of
* the minimum distance is ,
* the maximum distance is .

### STEP 2

As there is no background light the following values for the illuminance at the eye of the observer are chosen.

* minimum illuminance
* maximum illuminance

As the fairway is of minor importance the minimum visibility for calculation is set to

* (see 3).

### STEP 3

Calculate the in-situ-intensity with Allard’s law.

* minimum :
* maximum :
* design :

### STEP 4

Check for rival lights . The calculated intensity of is low compared to the relevant navigation lights of a passing vessel.

According to 6.2 and Table 4 the minimum intensity is set to

and in consequence the design intensity becomes

The maximum intensity stays unchanged.

### STEP 5

Photometric luminous intensity:

With and the photometric values are:

* minimum :
* maximum :
* design:

### Result

The lantern should have a photometric luminous intensity of approx. . The required minimum intensity is .

## Example 3

## Example 4

## Example 5

# LUMINOUS RANGE CALCULATION

The calculations described above have the aim to determine the photometric luminous intensity of a light from the required viewing distances . Range calculation is just the opposite way.

viewing distance

parameters

background illumination

rival lights

luminous intensity

in-situ / photometric

intensity calculation

Figure 9 Intensity calculation

measured luminous

intensity

Parameters

Flash profile

parametric range

nominal range

Figure 10 Range calculation

There are two purposes for a range calculation.

* Calculation of the nominal range for the list of lights and the nautical charts,
* Calculation of a parametric luminous range depending on meteorological visibilty and background illumination.

The initial value for all range calculation is the measured or calculated effective luminous intensity of the existing lantern. The service condition factor is considered in any case, so all calculations are based on .

## Calculation process

Allard’s law cannot be rearranged to calculate a distance directly . So the calculation of a range requires a numerical approximation, which is done by an iterative process.

Equation 14 Allard’s Law

### Newton-Raphson method

To determine the range from Allard’s law the Newton-Raphson method can be used. Therefore a function is defined as:

Equation 15 Function F

and the range is the root of the function .

Equation 16 Range as the root of function F

The iteration process is started with an initial guess of the range called .

A better approximation is then found with the value:

Equation 17 First step

This process is continued:

Equation 18 Step n+1

When the sequence of values do not differ much from each other, the process can be stopped and the last value of is found to be a good approximation for the range.

Equation 19 Final step

with a small value.

The derivative of is

Equation 20 Derivative

### Application to luminous range calculation

For range calculation the input values should be restricted to specific intervals to ensure that the iteration works (converges).

Practical limitations are:

Illuminance:

Visibility: ( to )

Luminous intensity:

For the initial guess should be set to .

The accuracy may be chosen as: .

Iteration:

* Start with
* Next value: -
* Loop until:
* Result : The last value of iteration process is the luminous range.

## Nominal Range

The nominal range is calculated with fixed values for visibility and illuminance.

Nominal range is defined for night and day time (link to new recommendation required).

* Nominal range for night time :  
  Visibility   
  Illuminance
* Nominal range for day time :  
  Visibility   
  Illuminance

The calculation is based on the effective intensity and takes into account a service condition factor of .

## Parametric luminous range

Any calculated luminous range, which is not a nominal range, should be named as a parametric range . As this value depends on the values for visibility and illuminance chosen, it is necessary to name these values when publishing a parametric range.

## Examples

A light was measured with an effective intensity of . Applying the service condition factor the in-situ-intensity will be .

Therefor the lantern has the following ranges:

* Night time nominal range:
* Day time nomianl range :
* Parametric range for and a Visibility :

1. Alternative Presentations of Allard’s Law

All calculations are based on Allard’s law. It calculates the illuminance of a signal light at the observer’s eye depending on the meteorological visibility and the distance between the light and the observer.

However very different presentations of this law are published. To avoid errors these different presentations are shown in the following sections.

The preferred version nowadays should use SI-units (International System of Units).

* 1. Physical presentation

A physical presentation of Allard’s law is given in Equation 21.

Equation 21 Allard’s Law, physical presentation

Where:

*E(d)* Illuminance at the eye of the observer

*I* Luminous intensity of the light

*z* exponential factor describing atmospheric absorption and scattering (extiction)

*d* distance between light and observer

In practice, there are alternative ways of characterizing the prevailing atmosphere as follows.

* 1. Allard’s lay using atmospheric transmissivity T

Atmospheric transmissivity (T) is defined as the ratio of the luminous flux transmitted by the atmosphere over a unit distance to the luminous flux which would be transmitted along the same path in a vacuum.

Equation 22 Transmissivity (luminous flux)

Where:

T atmospheric transmissivity (dimensionless)

luminous flux at the unit distance after passing through the atmosphere

theoretical luminous flux at the unit distance after passing through a vacuum

unit distance

Because the ratio of the luminous fluxes in Equation 22 is the same as the ratio of the corresponding illuminance values, Equation 22 can be rewritten as

Equation 23 Transmissivity (illuminance)

Where:

illuminance at the unit distance after passing through the atmosphere

theoretical illuminance at the unit distance after passing through a vacuum

Inserting expressions for and from Equation 21 into Equation 23, and noting that for , Equation 23 becomes

Equation 24 Transmissivity and exponential factor

Combining Equation 21 and Equation 24 yields

Equation 25 Allard’s law using transmissivity

* 1. Allard's law using the transmissivity TM for 1 nautical mile

The unit distance for transmissivity is chosen to be one nautical mile. Expressed in all metric units equation 5 takes the form

Equation 26 Allard's law using the transmissivity TM for 1 nautical mile

Where:

*E(d)* illuminance at distance d in metres

*I* luminous intensity in candela

*TM* atmospheric transmissivity [dimensionless] for 1 nautical mile

*d* distance in metres

*dU* unit distance that corresponds to the transmissivity [here: 1852 m]

In older publications the distance *d* is expressed in nautical miles. Using the fact that one nautical mile equals 1852 metres and suppressing the unit distance in the exponent Equation 26 can be written as

Equation 27

Where d is the distance in nautical miles.

Simplifying and suppressing all units yields

Equation 28 Allard’s law using nautical miles for the distance

Where:

*E(d)*  illuminance at the eye of the observer in lm/m2 [lx]

*I* luminous intensity of the light [cd]

*TM* transmissivity for one nautical mile of the atmosphere

*d* numerical value of the distance in nautical miles

* 1. Meteorological Visibility

The meteorological visibility is an alternative way to describe the extinction of the atmosphere, which in the development above is quantitatively characterised by the atmospheric transmissivity.

Meteorological visibility is the greatest distance at which a black object of suitable dimensions can be seen and recognized by day against the horizon sky, or, in the case of night observations, could be seen and recognized if the general illumination were raised to daylight level.

By definition the relationship between the meteorological visibility (*V*) and the transmissivity *TM* is

Equation 29 Meteorological visibility

Where:

*V* meteorological visibility in nautical miles

*TM* transmissivity [dimensionless] for one nautical mile

*dU* unit distance of 1 nautical mile

*ln* natural logarithm

Suppressing the unit distance yields:

Equation 30 Meteorological visibility in nautical miles

* 1. Allard’s Law based on Meteorological Visibility

It is recommended in the IALA dictionary that the atmospheric extinction be described by using meteorological visibility V rather than the transmissivity TM.

Allard's law can be expressed using meteorological visibility V by combining Equation 26 and Equation 29.

Equation 31 Allard’s law using meteorological visibility

Where:

*E(d)*  illuminance at the eye of the observer [lx]

*I* luminous intensity of the light [cd]

*d* distance in metres [m]

*V* meteorological visibility in metres [m]

In older publications the distance *d* and the visibility *V* are expressed in nautical miles. Equation 31 then becomes

Equation 32 Allard’s law using meteorological visibility and nautical miles

Where:

*E(d)* illuminance at the eye of the observer [lx]

*I* luminous intensity of the light [cd]

*d* distance in nautical miles

*V* meteorological visibility in nautical miles

the units (not shown) associated with (3.43×106) are m2/M2

1. References
2. CIE 18.2 The Basis of Physical Photometry ( International Commission on Illumination, 1983)
3. Convention on the International Regulations for Preventing Collisions at Sea, 1972 (COLREGs), International Maritime Organization
4. Convention on International Civil Aviation, Annex 14, Aerodromes, Volume 1, Aerodrome Design and Operations
5. ISO 16508:1999 / CIE S 006.1/E-1998 Road Traffic Lights - Photometric Properties of 200 mm Roundel Signals
6. CIE Publication No 43 Photometry of Floodlights
7. CIE Publication No 70 The Measurement of Absolute Intensity Distributions